

A Survey on State Estimation Techniques and Challenges in Smart Distribution Systems

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Abstract—This paper presents a review of the literature on state estimation (SE) in power systems. While covering some works related to SE in transmission systems, the main focus of this paper is distribution system SE (DSSE). This paper discusses a few critical topics of DSSE, including mathematical problem formulation, application of pseudo-measurements, metering instrument placement, network topology issues, impacts of renewable penetration, and cyber-security. Both conventional and modern data-driven and probabilistic techniques have been reviewed. This paper can provide researchers and utility engineers with insights into the technical achievements, barriers, and future research directions of DSSE.

Index Terms—Distribution system state estimation, pseudo-measurements, topology, cyber-security.

I. INTRODUCTION

DISTRIBUTION System State Estimation (DSSE) is the process of inferring the values of system's state variables using a limited number of measured data at certain locations in the system [1]. Thus, DSSE is basically a numerical process to map data measurements to state variables. While State Estimation (SE) is a well-developed and widely-used concept in transmission systems, its use at the distribution level is still the subject of active research. In recent years we have observed the rapid growth of Advanced Metering Infrastructure (AMI) in electric distribution systems (e.g., according to [2], the number of advanced meters in the U.S. was estimated to be 64.7 million devices in 2015, out of a total number of 150.8 million meters, indicating a penetration rate of 42.9%.) Hence, DSSE is expected to become a significant function in monitoring and power management of smart grids [3]. A general schematic of DSSE function is shown in Fig. 1. Extending conventional SE approaches to active distribution systems is a challenging

task due to several factors that are based on the considerable differences between the transmission and distribution systems:

- 1) *Observability problem*: Unlike transmission systems, the distribution systems are highly unobservable, meaning that the number of metering instruments in a network is generally small compared to the huge size of the system [4].
- 2) *Low x/r value*: In distribution systems, we generally face low x/r levels, which render the conventional DC SE techniques in transmission systems unusable at the distribution level [5].
- 3) *Unbalanced operation*: Distribution systems are in practice highly unbalanced which leads to a higher level of complexity in SE problem formulation.
- 4) *Communication issues*: Constraints on the communication system, such as the network bandwidth and capacity also limit the accuracy and rate of data exchange [6].
- 5) *Network configuration problem*: Considering the huge size of the distribution network and noting that the complete data related to the topology of this network is not commonly stored an additional degree of complexity to DSSE in these networks [7].
- 6) *Renewable energy integration*: The higher penetration of renewable power resources introduces a higher level of uncertainty in distribution system operation and DSSE.
- 7) *Cyber-security issues*: The issue of cyber-security is a new concern in management and control of active distribution systems.

Despite these challenges, industrial interest in implementing DSSE is growing. Electrical energy firms such as Eaton [8], Survalent [9], ETAP [10], OSI [11], and Nexant [12] have recently devised industrial programs for promoting system monitoring and management at the distribution level for utilities using DSSE. A discussion on relevant experiences on DSSE for radial distribution networks is presented in [13], where the connections between SE implementation and practical variables, such as line lengths, switch flows, voltage regulation, and measurement areas, are elaborated. In this paper we seek to present an extensive review of the proposed solutions to different DSSE-related problems. While the main focus of this paper is DSSE, certain works on transmission system SE have also been cited and reviewed where they become relevant. In summary, this paper discusses the following issues: DSSE problem formulation, pseudo-measurement generation, uncertain network topology, integration of renewable resources,

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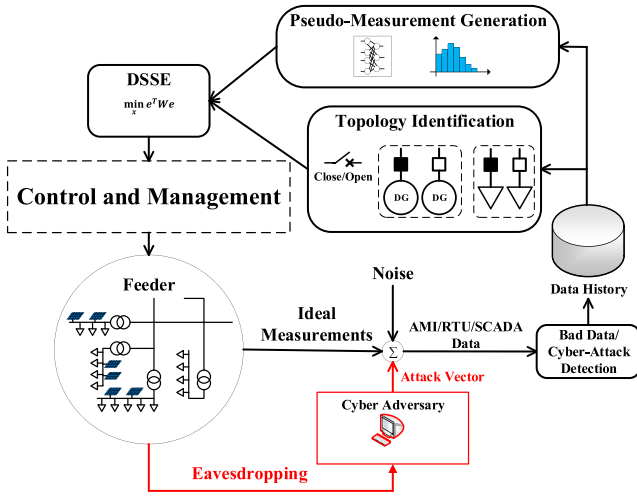


Fig. 1. DSSE function in smart grid environment.

79 meter placement, and DSSE cyber-security. Special attention
80 has been given to data-driven and machine-learning-based
81 approaches that are gaining interest to address different types
82 of problems [14].

83 The reviewed works address critical aspects of DSSE shown
84 in Fig. 1: 1) *DSSE solver module*: in Sections II and III, we
85 summarize the fundamentals of DSSE, with respect to choice
86 of algorithm and state variables. 2) *Pseudo-measurement gen-
87 eration module*: in Section IV the challenge of observability in
88 distribution systems and proposed pseudo-measurement gen-
89 eration solutions in the literature are elaborated. 3) *Topology
90 identification module*: Section V reviews the past works
91 related to online configuration tracking, connectivity detec-
92 tion, and topology discovery, which are pre-requisites for
93 obtaining accurate DSSE solutions. 4) *Feeder and instru-
94 mentation module*: The measurement units distributed across
95 the electric power system are the main sources of the infor-
96 mation for running the monitoring and control systems. In
97 Section VI, the problem of optimal meter placement and
98 potential PMU applications in distribution feeders is presented
99 in terms of practical constraints and objective functions.
100 Modern distribution feeders can have high penetration levels
101 of distributed renewable resources. The impacts of penetra-
102 tion of renewable energy resources in distribution feeders on
103 DSSE are analyzed in Section VII. 5) *Cyber-security module*:
104 Reliable DSSE depends on detection and prevention of cyber-
105 intrusions and cyber-attacks. The challenge of cyber-security
106 when performing wide-scale distribution system measurement
107 and monitoring is discussed in Section VIII. Furthermore,
108 conclusions and future research directions are provided in
109 Sections IX and IX-A.

110 II. FUNDAMENTALS OF SE

111 *A) Conventional Approach*: Given a measurement vector \mathbf{z}
112 (with size $m \times 1$), and a measurement function \mathbf{h} , which
113 connects the true state vector \mathbf{x} (with size $n \times 1$) to the
114 measurement vector (i.e., $\mathbf{z} = \mathbf{h}(\mathbf{x}) + \mathbf{e}$, with \mathbf{e} denoting the
115 measurement error vector), the state estimation problem can
116 be formulated as a Weighted Least Square (WLS) optimization

problem (with bold letters denoting vectors/matrices) [1]:

$$\hat{\mathbf{x}} = \arg \min_{\mathbf{x}} (\mathbf{z} - \mathbf{h}(\mathbf{x}))^T \mathbf{W} (\mathbf{z} - \mathbf{h}(\mathbf{x})) \quad (1)$$

where $\hat{\mathbf{x}}$ is the estimated state vector, T is the matrix transposi-
tion operation, and \mathbf{W} denotes the weight matrix that represents
the user's confidence in the measured data. A widely-used
choice for the weight matrix is $\mathbf{W} = \text{diag}\{\sigma_1^{-2}, \dots, \sigma_m^{-2}\}$,
where σ_j^2 represents the variance of the measurement error
corresponding to the j^{th} element of \mathbf{z} . This choice of the
weight matrix is based on two assumptions: 1) the error vec-
tor (\mathbf{e}) has a Gaussian distribution with zero mean, and 2) the
measurement errors of different elements of the measurement
vector are statistically independent. Under these assumptions
the WLS problem transforms to the maximum likelihood
estimation. A number of papers have deviated from the con-
ventional approach towards selecting \mathbf{W} . For instance, in [15],
using active/reactive power data history, non-diagonal terms
have been added to the weight matrix to obtain better WLS
accuracy, by modeling the existing correlation between the dif-
ferent measurement samples. This problem has been analyzed
in details in [16] for modeling the correlations in measure-
ment error distributions of different variables that are measured
by the same device (smart meters and PMUs.) For instance,
it is shown that the non-diagonal covariance terms between
different variables measured by the same device are as fol-
lows (notation: active power (P), reactive power (Q), voltage
magnitude (V), current magnitude (I), power factor ($\cos \Phi$):
 $\sigma_{V,P} = \sigma_V^2 I \cos \Phi$, $\sigma_{V,Q} = \sigma_V^2 I \sin \Phi$
 $\sigma_{P,Q} = \frac{1}{I} (\sigma_V^2 I^2 \sin 2\Phi - \sigma_\Phi^2 I^2 V^2 \sin 2\Phi + \sigma_I^2 V^2 \sin 2\Phi)$ (2)
Through another approach, in [17] and [18], the elements
of the diagonal \mathbf{W} matrix are updated using a weight func-
tion during solution iterations to obtain robustness against bad
data. The proposed weight updating mechanism for the i^{th}
measurement to obtain new weight value (\bar{w}_i) is as follows:

$$\bar{w}_i = \begin{cases} \sigma_i^{-2}, & D'_i \leq k_0 \\ \sigma_i^{-2} \zeta_i, & k_0 < D'_i \leq k_1 \\ 0, & D'_i > k_1 \end{cases} \quad (3)$$

where, D'_i , ζ_i , k_0 , and k_1 are parameters defined based on the
residual level corresponding to the i^{th} data sample. The idea
behind (3) is that as D'_i (which is a measure of low quality
of the measured data sample) increases beyond the introduced
thresholds (k_0 and k_1), the weight value assigned to it should
decrease (with factor ζ_i), reducing the influence of unreliable
or bad data samples on the outcome of the WLS.

Conventionally, Gauss-Newton method has been applied to
iteratively solve the WLS problem (1) [5]. This algorithm basi-
cally finds a solution to the equation $\nabla J = 0$, where J denotes
the objective function of optimization problem (1). The update
rules of the algorithm at the k^{th} iteration are as follows:

$$\mathbf{H}(\mathbf{x}(k)) = \frac{\partial J}{\partial \mathbf{x}(k)} \quad (4)$$

$$\mathbf{G}(k) = \mathbf{H}(\mathbf{x}(k))^T \mathbf{W} \mathbf{H}(\mathbf{x}(k)) \quad (5)$$

$$\Delta \mathbf{x}(k) = \mathbf{G}(k)^{-1} \mathbf{H}(\mathbf{x}(k))^T \mathbf{W} (\mathbf{z} - \mathbf{h}(\mathbf{x}(k))) \quad (6)$$

$$\mathbf{x}(k+1) = \mathbf{x}(k) + \Delta \mathbf{x}(k) \quad (7)$$

where, \mathbf{H} is the Jacobian of J with respect to the state variables, and \mathbf{G} is the system gain matrix. Other algorithms, such as back tracking method, trust region method, and quasi-Newton techniques, have also been applied instead of the classical Gauss-Newton method, to obtain better convergence properties [19]. Noting the non-convexity of (1) and the sensitivity of Newton method to initial conditions and gain matrix ill-conditioning, in [20] and [21], a Semi-Definite Programming (SDP) approach is proposed to find a good initial guess for the Newton method. The SDP formulation is based on the convex relaxation of the original WLS problem, which also guarantees the existence of a unique global solution. The computational efficiency of SDP is shown to be superior compared to that of the original non-convex problem. To further improve the computational performance of SDP-based SE, distributed algorithms have been employed for obtaining a solution [22].

Another modification in the structure of WLS (1) is the inclusion of *virtual measurements* as equality constraints ($\mathbf{c}(\mathbf{x}) = \mathbf{0}$). Virtual measurements represent operator's perfect information on certain aspects of system operation (e.g., zero-power-injection at nodes without customers.) Lagrange multipliers ($\boldsymbol{\lambda}$) have been proposed as penalty factors for enforcing these equality constraints [23]. The modified WLS objective function is defined as follows:

$$\{\hat{\mathbf{x}}, \hat{\boldsymbol{\lambda}}\} = \arg \min_{\mathbf{x}, \boldsymbol{\lambda}} (\mathbf{z} - \mathbf{h}(\mathbf{x}))^T \mathbf{W} (\mathbf{z} - \mathbf{h}(\mathbf{x})) + \boldsymbol{\lambda}^T \mathbf{c}(\mathbf{x}) \quad (8)$$

Given the above objective function, the state update step in the Gauss-Newton method (6) is changed to:

$$\begin{bmatrix} \Delta \mathbf{x}(k) \\ \boldsymbol{\lambda}(k) \end{bmatrix} = \begin{bmatrix} \mathbf{H}^T \mathbf{W} \mathbf{H} & \mathbf{C}(\mathbf{x}(k))^T \\ \mathbf{C}(\mathbf{x}(k)) & 0 \end{bmatrix}^{-1} \begin{bmatrix} \mathbf{H}^T \mathbf{W} (\mathbf{z} - \mathbf{h}(\mathbf{x}(k))) \\ -\mathbf{c}(\mathbf{x}(k)) \end{bmatrix} \quad (9)$$

where, $\mathbf{C}(\mathbf{x}) = \frac{\partial \mathbf{c}(\mathbf{x})}{\partial \mathbf{x}}$.

B) Alternative DSSE Structures: While WLS represents the conventional SE in power systems, alternative mathematical formulations have been proposed for the purpose of increasing the robustness of the state estimator when facing bad data. Noting the susceptibility of WLS to bad data, in [24], the use of Least Median of Squares (LMS) and Least Trimmed Squares (LTS) is studied, which shows improved behavior in handling outliers. Also, [25] investigates the use of Least Absolute Value (LAV) estimator, which has the property of automatic bad data rejection. Increasing the robustness of SE has also been promoted by using a Generalized Maximum-likelihood (GM) estimator instead of WLS in [26], where normalized residuals (r_n) are used through a convex score functions (denoted as $\rho(\cdot)$) in formulating the objective function. The SE formulation for these different approaches (including pros and cons) are shown in Table I, in terms of the objective function in optimization problem (1). In this table, the residuals $\mathbf{r} = [r_1, \dots, r_m]^T$ are defined as $r_i = z_i - h_i(\mathbf{x})$. Also, $med\{\}$ and $r_{(i)}$ define the set median and the i^{th} order statistics, respectively. Numerical comparisons of these alternative DSSE formulations in terms of robustness against system parameter uncertainties are presented in [27].

TABLE I
AVAILABLE ROBUST SE FORMULATIONS

Method	Objective Function	Pros and Cons
WLS	$\mathbf{r}^T \mathbf{W} \mathbf{r}$	(+) Fast, simple, widely-used, (-) Sensitive to bad data
LMS	$med\{r_1^2, \dots, r_m^2\}$	(+) Robust against bad data and leverage points, (-) High computational cost, high measurement redundancy requirements
LTS	$\sum_{i=1}^h r_{(i)}^2$	(+) Robust against bad data, (-) High computational cost and memory requirement
LAV	$\sum_{i=1}^m r_i $	(+) Robust against bad data, small sensitivity to line impedance uncertainty, (-) High computational cost, sensitivity to leverage points and measurement uncertainty
GM	$\sum_{i=1}^m \sigma_i^{-2} \rho(r_{n_i})$	(+) Robust against bad data, (-) Parameter selection sensitivity

Other approaches towards structuring the DSSE have been presented as well. For instance, some works in the literature tend to propose estimators which relax the Gaussian uncertainty assumption inherent to WLS. This is of practical importance given that this assumption is shown, through field tests, to be largely inaccurate [28]. Using Mean Squared Estimator (MSE) an analytic SE formulation is obtained in [29] which does not depend on Gaussian uncertainty assumptions and is capable of bad data measurement detection. A similar estimator is used in [30], where a Bayesian alternative to WLS is proposed. It is shown that the Bayesian approach has specifically better performance in presence of non-Gaussian uncertainty. Unlike WLS (equation (1)), the Bayesian approach tends to estimate states as a conditional averaging operation:

$$\hat{\mathbf{x}} = E\{\mathbf{x}|\mathbf{z}\} = \int \boldsymbol{\alpha} f_{\boldsymbol{\alpha}|\mathbf{z}}(\boldsymbol{\alpha}|\mathbf{z}) d\boldsymbol{\alpha} \quad (10)$$

Calculating $E\{\mathbf{x}|\mathbf{z}\}$ depends on our knowledge of the distribution function $f_{\mathbf{x}|\mathbf{z}}$, which can be obtained using Bayes rule, the measurement functions, and statistical properties of the system. Citing availability of accurate knowledge of second order statistics as a shortcoming of MSE-based methods, in [31] an alternative DSSE formulation is presented as a *matrix completion* problem which can be efficiently solved for billions of entries. Using information-theoretic reasoning it is shown that the optimal performance of DSSE is bounded by the capacity of AMI communication channels in charge of transmitting measurement samples to system operator.

To reduce the size of the optimization problem and speed up the convergence of WLS for large-scale feeders, in [32], the concept of quasi-symmetric impedance matrix is employed. This is achieved by adding the following constraint to the conventional WLS:

$$\begin{aligned} \min_{\mathbf{x}} & (\mathbf{z} - \mathbf{h}(\mathbf{x}))^T \mathbf{W} (\mathbf{z} - \mathbf{h}(\mathbf{x})) \\ \text{s.t.} & \mathbf{g}_0(\mathbf{x}) = \mathbf{x} - \mathbf{x}_0 - \mathbf{TRX} \cdot \mathbf{I}(\mathbf{x}) = 0 \end{aligned} \quad (11)$$

where, \mathbf{x} and \mathbf{x}_0 represent the voltage node state vector and the substation voltage, respectively. \mathbf{TRX} denotes the reduced impedance matrix and \mathbf{I} is the set of nodal current injections.

TABLE II
AVAILABLE DSSE FORMULATION STRUCTURES

Reference	Approach	State Variables	Pros and Cons
[33]	Voltage-based	Magnitude and phase angle	(+) Including general measurement functions, fast convergence, (-) State dependent and impedance-dependent Jacobian, radial topology only
[35]			(+) Linear formulation, non-iterative direct solution, applies to meshed topology, (-) Small angle difference assumption
[36]			(+) Branch-based formulation and computational efficiency, low sensitivity to network impedance, (-) Radial topology only
[34]		Real and imaginary parts	(+) State-independent Jacobian, (-) Need for obtaining current-based measurement functions, radial topology only
[32]			(+) High computational efficiency, applies to meshed networks, (-) Formulation complexity, impedance-dependency
[37]	Current-based	Real and imaginary parts	(+) Formulation and computational efficiency, phase-based decoupling in radial topology, impedance-independent Jacobian, (-) State-dependent Jacobian, exclusion of voltage measurements, phase-based coupling in meshed topology
[38]			(+) Phase-based and state-based decoupling for all topologies, efficient handling of current measurements, constant impedance, (-) Small angle difference assumption, exclusion of voltage measurements
[39][40]			(+) inclusion of voltage measurements, phase-based decoupling for radial topology, (-) State-dependent Jacobian
[41]		Magnitude and phase angle	(+) Efficient handling of current measurements, broad range of measurement functions, (-) State-dependent and impedance-dependent Jacobian
[42]		Magnitude/phase and real/imaginary	(+) Efficient handling of PMU data, (-) State- and impedance-dependent Jacobian, accuracy decline for meshed topology

III. DSSE PROBLEM FORMULATION

Due to the basic differences between transmission and distribution systems, the DSSE problem formulation can have major deviations from the conventional SE. The main point of difference is the modeling of measurement function (\mathbf{h}) in DSSE, as this function reflects the power flow equations in the power system. Hence, based on the choice of state and measured variables, choice of AC versus DC Power Flow (PF), and the representation of phases in power flow equations (for application in unbalanced systems), the measurement function can have different forms. In this section, we review the two basic formulations of DSSE (in terms of choice of state variables and measurement function) provided in the literature.

A) *Voltage-Based DSSE*: Traditionally, bus voltage magnitude and phase angle values have been used as state variables in transmission systems [1]. This conventional approach has also been employed in DSSE [33]–[36].

B) *Branch-Current-Based SE (BCSE)*: A notable group of works, have adopted branch current as state variables, which turns out to be a more natural way of DSSE formulation for distribution systems [37]–[42]. A summary of the properties of different DSSE formulations is shown in Table II.

IV. DISTRIBUTION SYSTEM OBSERVABILITY

“Observability” refers to the system operator’s ability to solve the state estimation problem. This depends on the number and location of metering instruments in the power system. Also, the availability and quality of critical measurement data samples in real-time has a crucial impact on power system

observability. Conventionally, numerical and topological methods have been used to assess the observability of transmission systems with respect to the number and location of meters, as demonstrated in [1]. Alternative observability assessment procedures have been employed at distribution level. For instance, in [43] a probabilistic approach is adopted to define an Unobservability Index (UI) as follows:

$$UI = \sum_{i=1}^n K_i = \sum_{i=1}^n \left(\sum_{j=1}^{B_i} -p(b_{i,j}) \log_2 p(b_{i,j}) \right) \quad (12)$$

where, K_i denotes the entropy of the i^{th} state (with $p(b_{i,j})$ defining the probability of the j^{th} bin for the i^{th} state.) Basically, UI represents our overall uncertainty on the distribution system state variable values. As another example, a graph-theoretic criterion for local observability assessment of distribution networks is obtained in [4].

Unlike transmission systems that enjoy a high level of data redundancy, the distribution systems are generally under-determined with poor observability. Thus, the accuracy of DSSE can be highly affected by the quality and availability of sensor data. The distribution system can easily become unobservable in case of communication failure/delays. Hence, bad/missing measurement data is closely connected to measurement redundancy and preserving the reliability of the DSSE problem. “Bad” data refer to data measurements that have considerable deviation from the underlying actual behavior, due to meter malfunction and communication noise. Missing data can also be treated as a special case of bad data. Conventionally, at the transmission level, bad data detection

TABLE III
AVAILABLE LITERATURE ON PSEUDO-MEASUREMENT GENERATION

Reference	Solution Approach	Pros and Cons	Load Estimation Model Input	Verification Approach
[45]	Probability density estimation using Beta functions	(+) Accurate empirical estimation, employing temporal load correlation, (-) Slow rate of convergence, radial only	Historic power consumption	Chi-square goodness of fit
[46] [47]	GMM	(+) Applicable to arbitrary load distributions, captures temporal load correlation, (-) Sensitivity to number of mixture components, expensive for high-dimensional learning	Standard load profiles, Historic data	
[48]	Statistical profile construction	(+) Captures temporal correlation, simple formulation, (-) Gaussian load distribution assumption		
[15]	Statistical power loss estimation	(+) Capturing temporal and spatial error correlations, (-) Gaussian error distribution assumption	Available measurements and estimated loss	Relative error in power loss and estimation outcomes
[6]	Statistical load variation modeling	(+) Captures load correlation at different time stamps, addresses non-synchronized measurement, (-) Gaussian estimation error distribution assumption	Smart meter data history, weather-related variables and load duration curve	Anderson-Darling test, Shapiro-Wilk test
[49]	Single Gaussian distribution	(+) Captures active/reactive power temporal correlation, (-) Gaussian load/estimation error distribution assumption		
[50]	PNN, clustering	(+) Applicable to arbitrary load distribution, captures correlation between consumption and economic code, (-) Sensitivity to cluster number		
[17]	PDP	(+) Robustness against measurement errors, corrective closed-loop system, (-) High computational cost		
[18]	NARX	(+) No a priori knowledge on load structure required, quickly adapts to changes in load pattern, (-) Gaussian load estimation error assumption		
[51]	Clustering, GMM	(+) Applicable to arbitrary load distributions, captures temporal (monthly) consumption correlations, (-) Sensitivity to cluster number, high computational cost, sensitivity to number of mixture components		
[52]	ANN, GMM	(+) Applicable to arbitrary estimation error distributions, (-) High computational cost, sensitivity to number of mixture components	Line flow measurements (generic consumption data)	DSSE relative error (voltage magnitude and phase), Bayesian information criteria

311 has been performed by inspecting the normalized measurement
312 residuals. However, this method is subject to failure and com-
313 plications in case of insufficient measurement redundancy and
314 multiple sources of bad data [1]. Hence, alternative approaches
315 have been employed to address this problem, along with the
316 sub-problem of missing data, at the distribution level (refer to
317 Section II.)

318 Hence, to improve the observability of distribution systems,
319 the input measurement set needs to be artificially augmented
320 (to compensate for missing data) or corrected (to compensate
321 for bad data.) This can be done through employing “pseudo-
322 measurement” samples, which are artificially-generated data-
323 points (e.g., active/reactive power, voltage and current, etc.)
324 based on the data history of the distribution systems [5]. A
325 basic approach is to use standard load profiles for generat-
326 ing pseudo-measurements [44]. Given that these data-points
327 are not highly accurate, they introduce high variance levels
328 in the weight matrix (\mathbf{W}), which could even lead to ill-
329 conditioning of the DSSE problem. Data-driven approaches
330 are employed for generating pseudo-measurements and han-
331 dling their uncertainty, including probabilistic and statistical
332 analysis, and machine-learning-based techniques.

333 *A) Probabilistic and Statistical Approaches:* Methods based
334 on probabilistic and statistical techniques, which employ spa-
335 tial/temporal correlation and historic probability distribution

336 data, are widely used for generating reasonable pseudo- 336
337 measurements and assessing their uncertainty. This includes 337
338 empirical studies [45], Gaussian Mixture Models (GMMs) and 338
339 Expectation Maximization (EM) [46], [47], time-varying vari- 339
340 ance and mean modeling [44], correlation analysis (between 340
341 total and individual consumption) [48], nodal active-reactive 341
342 correlation analysis [15], internodal and intranodal correlation 342
343 modeling [16], intertemporal correlation analysis [6], multi- 343
344 variate complex Gaussian modeling [49], and constrained 344
345 optimization [50]. 345

346 *B) Learning-Based Approaches:* Machine learning algo- 346
347 rithms have also attracted scientific attention in solving DSSE 347
348 problems, including addressing the problem of active/reactive 348
349 power pseudo-measurement generation and uncertainty assess- 349
350 ment. Probabilistic Neural Networks (PNNs) [51], Artificial 350
351 Neural Network (ANN) [52], clustering algorithms [53], 351
352 Parallel Distributed Processing networks (PDP) [17], and 352
353 Nonlinear Auto-Regressive eXogenous (NARX) [18]. 353

354 A summary of the notable papers in these two categories is 354
355 shown in Table III. Pseudo-measurement generation is basi- 355
356 cally a special type of load estimation at distribution level. 356
357 While there is a considerable number of works done in this 357
358 area, still unanswered questions remain. For instance, most 358
359 of the papers, instead of using real AMI data history, rely 359
360 on standard load profiles to perform numerical analysis and 360

361 verification. Also, the huge amount of data in practice can
 362 cause certain learning methods to become computationally
 363 expensive. Managing this “big data” challenge in distribution
 364 systems requires further research and studies.

365 V. NETWORK TOPOLOGY AND CONFIGURATION

366 The topology identification problem can be categorized into
 367 two separate, yet related, subproblems:

368 *A) System configuration identification:* The basic assumption
 369 within this set of problems is that the basic topology of the
 370 network is known to the system operator. However, due
 371 to local events (such as faults, line disconnections, switching
 372 events, etc.) the basic topology will undergo local changes over
 373 time. Limited knowledge of the operator on these changes
 374 will affect the accuracy of SE solutions. Hence, the objective
 375 is to use the system-wide measurements to update our
 376 knowledge of system configuration to avoid topology errors
 377 (i.e., state of switches, fuses, lines, DG/customer connection
 378 status.) Conventionally, generalized SE models have been
 379 used at the transmission level (with switch-related variables
 380 added to the SE formulation) to detect and correct topological
 381 errors [1], [54]. Similar classic methods have been
 382 applied to DSSE as well [55], [56]. Apart from the classical
 383 approaches, other probabilistic and data-driven methods
 384 have been applied for topology detection and identification in
 385 distribution systems. These methods are usually based on a
 386 data-driven search process in a limited topology space (i.e.,
 387 topology library) defined by variations on the basic topology,
 388 as shown in Fig. 2. Probabilistic recursive Bayesian
 389 approach [7], [57], fuzzy-based pattern recognition [58], auto-
 390 encoders [59], PMU voltage time-series [60], voting technique
 391 (“vote” for the best candidate structure) [61], correlation analysis
 392 [62], and maximum likelihood estimation [63], are a few
 393 of the proposed topology search methods.

394 *B) Topology learning:* Another set of problems are based
 395 on the assumption that the system operator has very limited
 396 or no knowledge of the basic topology of the network (which
 397 is highly applicable to the secondary distribution networks.)
 398 The objective is to discover the topology of the network by
 399 relying on nodal and branch measurements. Graph-theoretic
 400 algorithms have been used widely for topology discovery and
 401 learning considering different assumptions on system operator’s
 402 knowledge on topology. A sparse graph recovery model
 403 has been adopted in [64] to perform topology discovery, based
 404 on DC PF. The proposed method, which is based on nodal
 405 measurements, requires no *a priori* information on the topology
 406 of the network. Another data-driven graphical approach
 407 towards topology learning is proposed in [65]. In this work,
 408 an efficient graphical model is developed to represent the
 409 voltage magnitude dependencies (using mutual information as
 410 a measure of affinity) between neighboring buses (the basic
 411 assumption in this work is that current injections are statistically
 412 independent.) This method only depends on statistics of
 413 nodal voltage magnitude measurements (smart meter data) to
 414 reconstruct the partially or fully unknown radial or weakly-
 415 meshed topology. It is shown that for a radial feeder, the

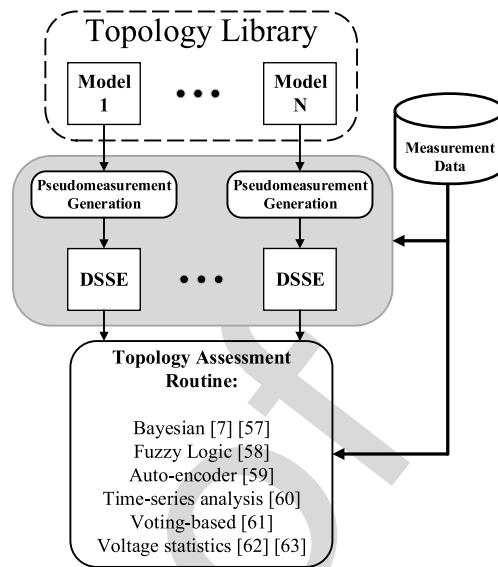


Fig. 2. Data-driven system configuration detection.

spanning tree that maximizes measures of internodal voltage
 mutual information corresponds to the true topology of
 the system. In [66], using nodal voltage measurements, the
 authors have been able to learn the topology of a radial
 feeder using mutual statistical properties of the measured variables.
 The proposed model is based on a linear approximation of lossless
 AC PF, and employs a bottom-to-top approach, in which the
 structure learning begins with the end nodes and moves towards
 the substation by choosing the proper parent nodes at each stage.
 The method is shown to have acceptable performance under a wide
 variety of assumptions, including no prior knowledge on the basic
 topology and missing measurement data. In [67], graph-theoretic
 interpretation of principal component analysis and energy conservation
 are employed in the context of graph theory to obtain radial
 distribution system topology through smart meter energy usage
 data. A more general approach (applicable to meshed networks
 even with missing PMU phase measurements) for estimating both
 the topology of the network and the line parameters is proposed
 in [68], where the line parameters and system topology are
 updated consecutively through an EM-based approach. Starting
 with an initial topology guess, at each step of the algorithm,
 the topology is updated by removing edges with small estimated
 susceptance values to improve the estimation likelihood.

441 VI. DISTRIBUTION NETWORK METERING 442 SYSTEM DESIGN AND ANALYSIS

443 A. Metering Instrument Placement

444 Optimizing the location of metering instruments in distribution
 445 systems is a significant subject for research, given the size of
 446 the system and potentially limited financial resources [69].
 447 Different objectives have been proposed in the literature to
 448 address this problem, including improving system observability,
 449 minimizing installation/maintenance costs, bad data detection
 450 capability, and improving the DSSE

TABLE IV
METER PLACEMENT METHODS

Reference	Objective Function	Constraints	Solution Algorithm
[69]	Meter cost	Estimation accuracy	Heuristic search
[70] [71]	Estimation accuracy	X	Ordinal optimization
[72][73]	Meter cost, Estimation accuracy	Estimation accuracy	GA
[74]	Estimation accuracy	X	GA
[75]	Determinant of the overall Fisher information matrix	Meter number	Boolean-convex optimization
[76][77]	Estimation accuracy	Meter number	MISDP
[78]	Estimation accuracy	Meter number	Submodular saturation algorithm
[43]	Network observability	X	Heuristic search
[79]	Meter cost, estimation accuracy	Estimation accuracy	MOE

accuracy [41], [43], [70]–[80]. Different algorithms have been tried for solving the placement problem, including Genetic-Algorithm (GA), Mixed Integer Linear Programming (MILP), Mixed Integer Semi-Definite Programming (MISDP), and Multi-Objective Evolutionary (MOE) methods. A summary of the different meter placement approaches is given in Table IV.

B. PMU Applications and Impacts on DSSE

PMUs are able to provide synchronized voltage, power, and current measurements that enable accurate tracking of state variables and efficient control and management decisions. Also, generally the sampling frequency of PMUs (up to 30 kHz) is much higher than that of smart meters (0.277 mHz - 16.7 mHz), which leads to system observability on a higher temporal granularity. However, compared to smart meters, the use of PMUs in distribution networks is still very restricted due to their prohibitive costs. Hence, a critical research direction related to PMUs is optimizing the number and location of PMUs to enhance system observability, while limiting the measurement infrastructure costs [81] (also see Section VI-A).

In terms of application in distribution systems, PMUs have been employed for high-resolution voltage/power profiling, oscillation detection, topology identification, and event detection, as outlined in [82]. On the other hand, smart meters have been used mostly for low-resolution load forecasting and management, and connection verification [83]. In terms of algorithm design for DSSE and topology identification, one considerable difference between the methods proposed for systems with only smart meters and systems with PMUs is the “small phase angle difference assumption”. Hence, due to unavailability of phase angle data in absence of PMUs many papers have assumed that the nodal voltage phase angles in a system are almost equal [65], [66], [84]. While this assumption introduces bounded inaccuracies in the final estimation/identification outcomes, it enables system operators to monitor the state of distribution systems without PMUs. Furthermore, adding the voltage phase data or flow measurements can highly improve the estimation and identification routines’ performance.

VII. PENETRATION OF RENEWABLE RESOURCES

A few papers have analyzed DSSE under high penetration rates of renewable power. The main source of challenge in performing SE in presence of renewable resources is their uncertain output power [85]. Also, deep penetration of renewable power sources affect the voltage profile of distribution systems. This stresses the need for more advanced voltage monitoring capabilities [50]. In case of pseudo-measurement generation for these resources, it is believed that the non-Gaussian distribution of renewable power would adversely affect conventional WLS-based DSSE methods. Moreover, as shown in [14], fast changes in system state can result in the WLS-based DSSE to get trapped in local minima with errors as high as 10^5 times the underlying global solution. Also, given that the performance of conventional Gauss-Newton algorithm highly depends on the initial conditions, finding good initial conditions for DSSE in systems with deep renewable penetration is a difficult task [4]. To address these challenges several papers have adopted different approaches for solving the SE (in general) and DSSE (in particular) in presence of renewable-based DGs.

Probabilistic methods represent the major group of techniques for modeling the impacts of renewable uncertainty on SE. A forecasting-aided SE mechanism is proposed in [86] to capture the temporal and spatial correlation among DGs and loads for their short-term prediction (to be used as pseudo-measurements in SE), using a linear autoregressive model. In [29], another forecasting-aided SE method is proposed to manage the uncertainties of load and renewable resources based on a GMM technique for obtaining the non-Gaussian distribution of renewable power while incorporating the dynamics of the system. Moreover, this estimator shows good performance even with limited data, which makes it a promising candidate for DSSE. As an extension to [73], the effect of the uncertainty of renewable DG power profile on meter placement has been modeled in [87] using GMM. A probabilistic graphical modeling technique has been proposed in [88] for capturing short term uncertainty of SE in systems with high PV penetration. The physical governing laws of the system (i.e., PF equations) have been embedded into the SE model. A distributed belief propagation method is performed for state inference, which yields superior results compared to the conventional deterministic WLS method. Another probabilistic approach is adopted in [44] for pseudo-measurement generation in networks with high residential PV penetration using Beta distribution functions. It is speculated that the uncertainty of PV systems has the highest impact on the DSSE at mid-day time intervals (when usually the load profile is not peaking.) To model the non-Gaussian uncertainty of PV power in DSSE, pseudo-measurements are generated (with 15-minute time resolution) for roof-top dispersed PV systems employing a weather-dependent model for constructing general PV power probability density functions, considering solar radiation, temperature, number of arrays and their physical characteristics. This approach shows considerable improvements on DSSE accuracy compared to using conventional standard profiles. While in [44] the possible correlation between physically nearby renewable DGs are not modeled, it is demonstrated

TABLE V
AVAILABLE LITERATURE ON SE CYBER-SECURITY

Reference	Topic	System Model	Attacker Model	Model Constraints	Proposed Countermeasures
[89]	False data injection	DC PF	Full system knowledge	Limited resource and meter access	Spatial and temporal-based detection
[90]			Limited topology knowledge		Generalized likelihood ratio detector
[91]		AC and DC PF	Full system knowledge	Detectability constraints	Load shift factor monitoring
[94]	Local state knowledge		Limits on system loss knowledge	X	
[97]	Local system information		Noisy measurements	Cover-up meter protection strategy	
[98]	Wide range of system knowledge		Access to the Jacobian matrix	Topology information masking	
[99]	Topology Attack	AC PF	Full system knowledge	Limited resource	Generation forecasting
[95]				Unlimited access to all meters	X
[15]	Data Privacy	Linear Dynamic	X	Limited access to smart meters	Smart meter data aggregation
[100]			Monitoring control signals	Gaussian noise assumption	Proper channel capacity assignment

in [16] that including the correlation between close DGs for pseudo-measurement generation leads to further improvements in DSSE accuracy.

VIII. CYBER-SECURITY

The vulnerability of the power system against cyber-attacks has been observed in practice. Different types of cyber-attack related to SE have been modeled and investigated in the literature: false data injection, topology attacks, and eavesdropping. In a false data injection situation, an attacker, with various degrees of knowledge on system parameters and states, alters the metered data of certain metering devices [89]–[94]. In a topology attack, the attackers tend to maliciously modify the topology model data of the system [95]–[99]. Eavesdropping defines a situation in which an unauthorized party seeks to gather system data by tapping into the communication infrastructure, compromising data privacy and confidentiality of users [15], [100]. A classification of different papers with respect to the issue of cyber-security can be seen in Table V. It can be concluded that protecting the vital automation and monitoring systems against cyber intrusion and cyber attacks requires a holistic approach to preserve the integrity, availability, and confidentiality of DSSE at all times. Different components of an effective solution include: adversary identification (in terms of knowledge and resource levels), vulnerability assessment (critical meters, communication system integration, sensitivity of DSSE to bad data), and personnel training.

IX. CONCLUSION

In this paper, we have presented an overview of the critical aspects of DSSE. Active research subjects, such as DSSE problem formulation, pseudo-measurement generation, network topology, data meter placement, renewable resource integration, and cyber-security are reviewed. Based on the survey, most recent works are more concentrated on using data-driven and machine-learning-based modifications in the conventional DSSE (for improving the accuracy, robustness, and system observability), which is a reasonable direction given the steep increase in the rate of installation of smart

meters and micro-PMUs at the distribution level. Probabilistic modeling (in a data-driven context) has also attracted substantial research works, due to its capability for capturing the effects of stochastic and variable renewable resources on active distribution systems in general (and on DSSE in particular.)

A. Future Research Directions

It would be of interest to study how Demand Response (DR) programs [101] could impact the DSSE (in terms of uncertainty and variability of customer behavior and pseudo-load generation) by incorporating retail market signals into the DSSE problem formulation. In general, integrating the price-sensitivity of active distribution networks into the DSSE becomes a valid research problem in future distribution systems with deep penetration of renewable and DR resources. In a related context, optimal power management and decision making under limited distribution system observability appears to be a largely unexplored direction for research, specially in presence of emergent technologies, such as energy storage systems and networked microgrids [102]–[105]. Another very recent area of interest is topology learning. Future research is needed to discover if and how topology discovery can be performed after extreme weather events [106] as the number of data meters decreases due to communication and device failure, and the observability of the distribution system is compromised. Employing data-driven methods under extreme weather events at different stages (pre-event, during the event, and post-event) for developing system monitoring and learning techniques is another possible research direction. Thus, it would be of interest to investigate the impact of extreme events on distribution system observability and design potential solution strategies to enable effective system restoration strategies that depend on operator’s real-time knowledge of system states.

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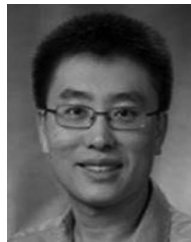
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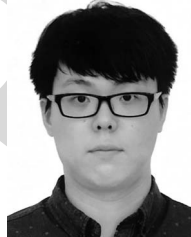
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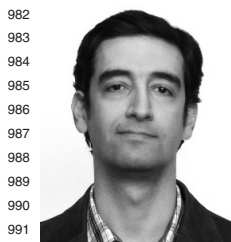
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