

Enriching Load Data Using Micro-PMUs and Smart Meters

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Abstract—In modern distribution systems, load uncertainty can be fully captured by micro-PMUs, which can record high-resolution data; however, in practice, micro-PMUs are installed at limited locations in distribution networks due to budgetary constraints. In contrast, smart meters are widely deployed but can only measure relatively low-resolution energy consumption, which cannot sufficiently reflect the actual instantaneous load volatility within each sampling interval. In this paper, we have proposed a novel approach for enriching load data for service transformers that only have low-resolution smart meters. The key to our approach is to *statistically* recover the high-resolution load data, which is masked by the low-resolution data, using trained probabilistic models of service transformers that have both high- and low-resolution data sources, i.e., micro-PMUs and smart meters. The overall framework consists of two steps: first, for the transformers with micro-PMUs, a Gaussian Process is leveraged to capture the relationship between the maximum/minimum load and average load within each low-resolution sampling interval of smart meters; a Markov chain model is employed to characterize the transition probability of known high-resolution load. Next, the trained models are used as *teachers* for the transformers with only smart meters to decompose known low-resolution load data into targeted high-resolution load data. The enriched data can recover instantaneous load uncertainty and significantly enhance distribution system observability and situational awareness. We have verified the proposed approach using real high- and low-resolution load data.

Index Terms—Distribution system, load uncertainty, micro-PMU, smart meter, data enrichment.

I. INTRODUCTION

AS THE advanced metering infrastructure (AMI) has been widely deployed in distribution systems in recent years, utilities have gained access to large amounts of smart meter (SM) data [1]. To take advantage of this data, which is both spatially and temporally fine-grained, researchers and industry practitioners have performed time-series power flow

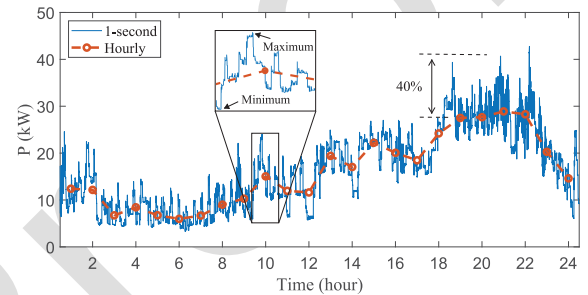


Fig. 1. A one-day real service transformer load curve with 1-second load data and the corresponding hourly average load curve.

studies for optimizing network operation, expansion [2], [3], and integrating renewable energy resources [4]. In many cases, customer-level demands are aggregated to obtain service transformer-level loads for performing power flow studies [2], [5]. However, the problem is that in most cases, SMs have a low sampling rate, e.g., one to four samples per hour. Thus, the average demand measured at such low resolutions cannot faithfully represent the uncertainties of the instantaneous load. As illustrated in Fig. 1 for an exemplary transformer, the maximum 1-second load data has reached values 40% times larger than the corresponding hourly SM reading within the same sampling interval. Also, compared to the hourly measurements, the instantaneous load shows a high level of variability, which has not been captured by the SMs. Therefore, recovering the *masked* high-resolution load data is critical in enhancing distribution system situational awareness and granularity of modeling.

To further demonstrate the usefulness of high-resolution load data, we primarily focus on three specific applications. *First*, accurate power flow analysis requires high-resolution load data. Power flow analysis is critically important for utilities. It can provide voltage profiles, which can help utilities plan new circuits, add customers, and track and fix voltage problems. Since load is an essential component in distribution systems, high-resolution load profiles play a critical role in obtaining power flow solutions with high fidelity. In contrast, the 15-min, 30-min, or 1-hour load data might cause unacceptable errors [6], [7]. This is why most utilities take conservative approaches in distribution system operation and planning. Instead, taking full advantage of high-resolution load data can free utilities from conservative measures. *Second*, accurate voltage regulation analysis requires high-resolution

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69 load data. In many cases, utilities perform time-series power
 70 flow analysis to examine the actions of voltage regulation
 71 devices. Typical voltage regulation devices include voltage
 72 regulators and capacitors. The controller of these two types of
 73 devices usually has a time delay before executing a regulating
 74 order. By doing this, the voltage regulation devices can avoid
 75 unnecessary frequent reactions to fast and temporary voltage
 76 transients. The time delay is typically around 30 seconds.
 77 Therefore, to accurately capture the response of voltage regu-
 78 lation devices, the time resolution of load data for performing
 79 time-series power follow analysis should match the delay time
 80 of regulation devices' controller [6], [8]. *Third*, high-resolution
 81 load data can facilitate photovoltaic (PV) integration. In most
 82 cases, utilities conservatively maintain customer voltages very
 83 close to the upper bound of the ANSI voltage range due to
 84 conservative considerations. Under this condition, even though
 85 the load increase may cause a voltage drop, the voltage will
 86 still be within the ANSI voltage range and satisfy voltage qual-
 87 ity requirements. However, under such conservative operation
 88 logics, new PV integration can cause over-voltages. To assess
 89 the impact of PV generation, one promising way is to uti-
 90 lize high-resolution (1-second or 1-min) PV generation data
 91 to perform power flow analysis, because low-resolution data
 92 might fail to capture PV output variations. Since the load varia-
 93 tions might not be negligible in some scenarios, it is necessary
 94 to combine high-resolution load data and PV output data to
 95 perform time-series power flow analysis [9], [10].

96 There is only a limited number of previous works focus-
 97 ing on load data enrichment. In [8], a top-down method is
 98 presented to generate service transformer-level high-resolution
 99 load profiles. First, low-resolution substation load profiles
 100 are allocated to service transformers via scaling. Then, the
 101 allocated profiles are decomposed into high-resolution load
 102 data by aggregating typical load patterns stored in variabil-
 103 ity and diversity libraries. In [11], synthetic load datasets are
 104 created for four typical seasonal months using captured vari-
 105 ability from high-resolution service transformer load data. To
 106 develop rich load data, researchers have added random noise to
 107 load data for modeling load uncertainty, as presented in [12].
 108 In [13], a discrete wavelet transform (DWT)-based approach
 109 is proposed to parameterize intra-second variability of high-
 110 resolution transformer load data. To sum up, the primary
 111 limitations of previous load data enrichment methods are: the
 112 scaled substation load profiles allocated to service transformers
 113 differ from the actual load profiles since each transformer has a
 114 distinct load pattern [14], inaccuracy of adding random noise,
 115 and lack of specific methodology for applying the extracted
 116 load variability [7].

117 Considering the shortcomings of previous works, in this
 118 paper, we have developed a novel *bottom-up* approach for
 119 enriching hourly load data for service transformers that only
 120 have SMs, by leveraging the high-resolution load data of ser-
 121 vice transformers with micro-PMUs and SMs. This concept is
 122 illustrated in Fig. 2, where the service transformer in the mid-
 123 dle with rich load data is utilized to perform load data enrich-
 124 ment for the other two service transformers with only SMs.
 125 Before proceeding to specific steps, we have observed that
 126 each low-resolution load observation corresponds to a *segment*

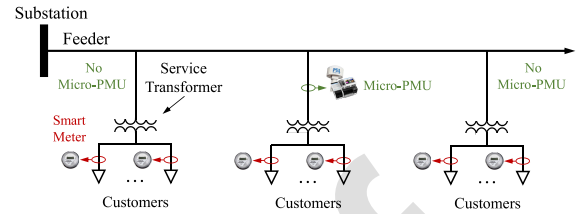


Fig. 2. Schematic diagram of a radial distribution feeder with diverse sensors.

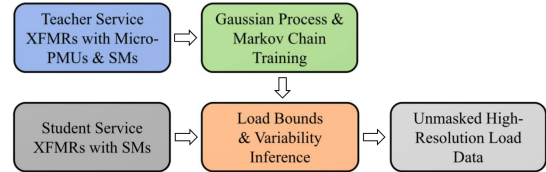


Fig. 3. Overall structure of the proposed load data enrichment approach.

of high-resolution load profile, as shown in Fig. 1. Therefore,
 enriching one known low-resolution load observation comes
 down to determining the maximum and minimum loads in the
 corresponding high-resolution load profile segment and infer-
 ring how the instantaneous load varies within those bounds. To
 do this, the proposed approach exploits learned probabilistic
 models that are trained using the high-resolution load data of
 service transformers *with* micro-PMUs. Thus, the first stage is
 to train probabilistic models using known high-resolution load
 data of micro-PMUs. Specifically, a Gaussian Process is used
 to capture the relationship between the maximum/minimum
 bound and the average load. A Markov process is leveraged to
 model the probabilistic transition of instantaneous load within
 the bounds. These trained models for transformers with micro-
 PMUs form a *teacher* repository. The second stage is to extend
 the trained probabilistic models to the service transformers that
 only have SMs, i.e., the *students*, for enriching low-resolution
 load data. Specifically, the trained Gaussian Process models
 are employed to estimate the unknown maximum/minimum
 bound using the known low-resolution observation as the
 input, and the trained Markov models are used to probabilis-
 tically determine the variability of instantaneous load within
 the estimated maximum and minimum bounds. In addition, the
 load enrichment process in the second stage is performed using
 a weighted averaging operation, where the weights are deter-
 mined by evaluating the similarity between low-resolution load
 data of the student and teacher transformers. Our approach
 is not restricted to the condition that the teacher and stu-
 dent transformers should have the same rating, loss, or served
 customer number. The overall framework of our proposed
 approach is illustrated in Fig. 3.

The primary contribution of our paper is that we have
 proposed a novel bottom-up inter-service-transformer load
 data enrichment approach using micro-PMUs and SMs. Our
 method takes full advantage of the fine-grained spatial and
 temporal granularity of SM and micro-PMU data. The rest
 of the paper is organized as follows: Section II presents the
 process of training teacher models using data from transfor-
 mers with micro-PMUs. Section III describes the procedure of
 enriching load data for transformers with only SMs using

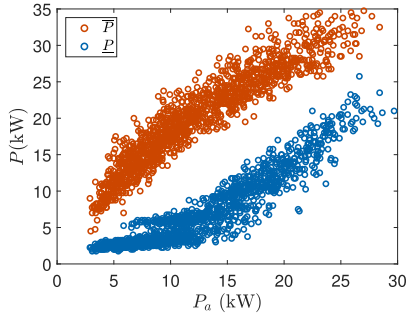


Fig. 4. Observation from real high-resolution load data for a service transformer.

the trained teacher models. In Section IV, case studies are analyzed, and Section V concludes the paper.

II. CONSTRUCTING A REPOSITORY OF TEACHER TRANSFORMERS

The first step in load data enrichment is to train inference models based on high-resolution micro-PMU load data. In this section, inference model training includes two stages: load boundary inference model training, and load variability parameterization. Also, keep in mind that the inference model training process is performed for *each* service transformer with a micro-PMU.

A. Training Load Boundary Inference Model

Based on real high-resolution load data, we have observed that the average load over each low-resolution sampling interval, P_a , and the corresponding maximum/minimum load within that interval demonstrate a nonlinear relationship, as shown in Fig. 4. Note that \bar{P} and \underline{P} denote the upper and lower bounds of instantaneous load within each sampling interval, respectively. Considering this, the Gaussian Process regression (GPR) technique, which shows excellent flexibility in capturing nonlinearity, is leveraged to train load boundary inference models [15]. One primary reason for choosing GPR is that after running numerical tests, it demonstrated a relatively better performance when applied to our dataset than some other state-of-the-art nonlinear regression models, such as the Support Vector Machine model and the Polynomial regression model. Note that other regression models with acceptable accuracy can also be integrated into our proposed framework for load data enrichment. The basic idea behind GPR is that if the distance between two explanatory variables is small, we have high confidence that the difference between corresponding dependent variables will be small as well. Specifically, using GPR, the upper bound of instantaneous load within the t 'th hour, $\bar{P}(t)$, as a function of the hourly average load can be written as:

$$\bar{P}(t) = f(P_a(t)), \quad (1)$$

where, $P_a(t)$ denotes the average load over the t 'th hour. Unlike deterministic approaches, where $f(P_a(t))$ is assumed to yield a single value for each $P_a(t)$, in GPR, $f(P_a(t))$ is a random variable. Intuitively, the distribution of $f(P_a(t))$ reflects

the uncertainty of functions evaluated at $P_a(t)$. In GPR, the function $f(P_a(t))$ is distributed as a Gaussian process:

$$f(P_a(t)) \sim \mathcal{GP}(\mu(P_a(t)), K(P_a(t), P_a(t'))), \quad (2)$$

where, $\mu(P_a(t))$ reflects the expected value of the maximum load inference function, and the covariance function $K(P_a(t), P_a(t'))$ represents the dependence between the maximum loads during different hour intervals. In our problem, the covariance function $K(\cdot, \cdot)$ is specified by the Squared Exponential Kernel function expressed as:

$$K(P_a(t), P_a(t')) = \sigma_f^2 \exp\left(-\frac{\|P_a(t) - P_a(t')\|_2^2}{2\lambda^2}\right), \quad (3)$$

where, $\|\cdot\|_2$ represents l_2 -norm, σ_f and λ are hyper-parameters, which are determined using cross-validation. Intuitively, (3) measures the distance between $P_a(t)$ and $P_a(t')$, which can also reflect the similarity between $\bar{P}(t)$ and $\bar{P}(t')$, as shown in Fig. 4. For each service transformer with a micro-PMU, the average load and corresponding maximum load during each hour interval are known and provide a training dataset. Thus, applying (2) to the entire training dataset consisting of N hourly average and maximum load pairs, $\{(P_a(1), \bar{P}(1)), \dots, (P_a(N), \bar{P}(N))\}$, an N -dimensional joint Gaussian distribution can be constructed as:

$$\begin{bmatrix} f(P_a(1)) \\ \vdots \\ f(P_a(N)) \end{bmatrix} \sim \mathcal{N}(\boldsymbol{\mu}, \boldsymbol{\Sigma}), \quad (4)$$

where,

$$\boldsymbol{\mu} = \begin{bmatrix} \mu(P_a(1)) \\ \vdots \\ \mu(P_a(N)) \end{bmatrix}, \quad (5a)$$

$$\boldsymbol{\Sigma} = \begin{bmatrix} K(P_a(1), P_a(1)) & \cdots & K(P_a(1), P_a(N)) \\ \vdots & \ddots & \vdots \\ K(P_a(N), P_a(1)) & \cdots & K(P_a(N), P_a(N)) \end{bmatrix}. \quad (5b)$$

The joint Gaussian distribution formulated in (4) represents a trained nonparametric *maximum* load inference model. Also, the same procedure can be applied to the hourly average and minimum load pairs, $\{(P_a(1), \underline{P}(1)), \dots, (P_a(N), \underline{P}(N))\}$, to obtain a trained nonparametric *minimum* load inference model.

In summary, for each service transformer with a micro-PMU, we can obtain two trained GPR models for inferring the maximum and minimum loads based on the corresponding hourly average load measured at the low-resolution sampling intervals.

B. Training Load Variability Inference Model

Given an hourly average load observation, simply determining load boundaries is not sufficient for load data enrichment. We also have to learn how the load varies within these bounds. It is observed from real high-resolution load data that when an appliance is turned on, the load will jump to a certain level, as shown in Fig. 5. This process can be modeled as the Markov chain, which represents a system transitioning from one state

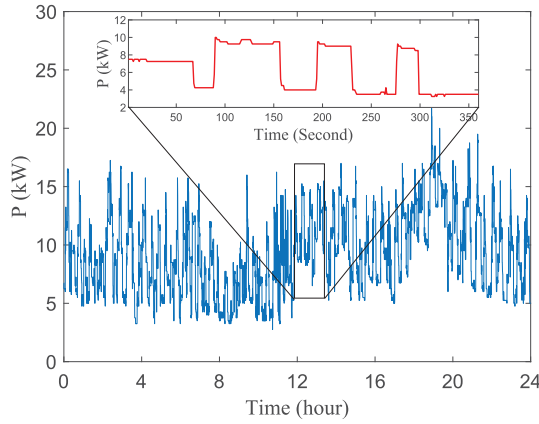


Fig. 5. Load variations within a day captured by high-resolution data.

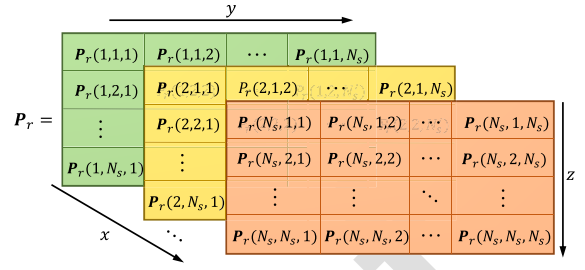


Fig. 6. Representation of the 3D probability transition matrix.

$$\text{if } F\left(\frac{(j-1) \times 100}{N_d}\right) \leq P_a(t) < F\left(\frac{j \times 100}{N_d}\right), \quad (7) \quad 288$$

where, $F(\cdot)$ is a function that returns percentiles of the entire 289 set of low-resolution load observations, and N' is the total 290 number of discretized observation states in each low-resolution 291 sampling interval. 292

Then, for each subset \mathbf{D}_j , the stochastic process is parame- 293 terized by empirically estimating the transition probabilities 294 between discrete observed states in terms of a transition 295 matrix. A second-order Markov process consists of three 296 states: the previous state, the current state, and the next state. 297 Therefore, the stochastic transition matrix, \mathbf{P}_r , is a three- 298 dimensional (3D) array, as illustrated in Fig. 6. Each element 299 of \mathbf{P}_r , $\mathbf{P}_r(x, y, z)$, represents the probability of moving to state 300 z under the condition that the previous state is x and the current 301 state is y . For each subset \mathbf{D}_j , elements of \mathbf{P}_r can be estimated 302 from the frequencies of posterior states. Assume \mathbf{D}_j takes on 303 the form of $\{S(i), i = 1, \dots, N'_s\}$, where N'_s is the total num- 304 ber of observation states in \mathbf{D}_j , then the occurrence number at 305 (x, y, z) can be counted as: 306

$$\mathbf{n}(x, y, z) = \sum_{i=2}^{N'_s-1} [S(i-1) == x \text{ and } 307 S(i) == y \text{ and } S(i+1) == z], \quad (8) \quad 308$$

where, $[\cdot]$ is the Iverson bracket which converts any logical 309 operation into 1, if the operation is satisfied, and 0 otherwise. 310 “==” stands for the “equal to” operator and “and” is the log- 311 ical and operator. Thus, the elements of transition probability 312 matrix are computed by: 313

$$\mathbf{P}_r(x, y, z) = \frac{\mathbf{n}(x, y, z)}{\sum_z \mathbf{n}(x, y, z)}, \quad x, y = 1, \dots, N_s. \quad (9) \quad 314$$

For each subset $\mathbf{D}_j, j = 1, \dots, N_d$, (9) is performed to obtain 315 a 3D stochastic transition matrix. Moreover, for each service 316 transformer with a micro-PMU, the entire above-mentioned 317 procedure for parameterizing variability is conducted to obtain 318 N_d stochastic transition matrices. 319

III. ENRICHING LOAD DATA FOR TRANSFORMERS WITH 320 ONLY SMART METERS 321

A. Determining Teacher Weights 322

Recall that our goal is to recover the high-resolution load 323 data masked by the low-resolution load data. In this procedure, 324 we leverage teacher models of transformers with micro-PMUs 325 for service transformer with only SMs. Note that there might 326

251 to another over time. Also, it is observed from Fig. 5 that once 252 the load has transitioned to a certain level, it will stay almost 253 invariant for a certain period of time. Therefore, the load state 254 duration demonstrates statistical properties, and there exists a 255 temporal correlation in state transition. Considering this, we 256 have employed a second-order Markov model to capture the 257 stochastic variability of the instantaneous load. Markov chains 258 of second order are processes in which the next state depends 259 on two preceding ones.

Since load is continuous, the first step to parameterize a 260 Markov chain process is to discretize *high-resolution* load 261 measurements. Specifically, for the i 'th high-resolution load 262 observation during the t 'th hour interval, the corresponding 263 observed state is determined as:

$$S_t(i) = n_s, \quad n_s \in \{1, \dots, N_s\}, t = 1, \dots, N, 265 \\ \text{if } (n_s - 1) \frac{\bar{P}(t) - \underline{P}(t)}{N_s} \leq P_t(i) - \underline{P}(t) < n_s \frac{\bar{P}(t) - \underline{P}(t)}{N_s}, 266 \quad (6) \quad 267$$

268 where, N_s represents the total number of the unique discrete 269 states and $P_t(i)$ is the i 'th instantaneous load measurement 270 during the t 'th hour.

271 Also, it is observed from real high-resolution load data 272 that different load levels display different stochastic processes. 273 Typically, an air-conditioner cyclically starts and stops in 274 the order of minutes. In contrast, the baseload, which is 275 often caused by lighting and electronic devices, shows signif- 276 icantly longer cycles. In addition, the air-conditioning devices 277 and baseload appliances show different average load levels 278 over low-resolution sampling intervals due to different capaci- 279 ties. Therefore, to capture the different transition processes, 280 the discretized observation states need to be divided into 281 multiple subsets according to the hourly average load mea- 282 surements. Each subset is used to train a Markov chain 283 model. Specifically, first, the entire collection of discretized 284 observation states is split into N_d subsets according to the 285 corresponding low-resolution load observation, $P_a(t)$. The j 'th 286 subset is obtained as:

$$\mathbf{D}_j = \{S_t(i)\}, \quad i \in \{1, \dots, N'\}, t \in \{1, \dots, N\}, 287$$

be more than one teacher transformer serving the same number of customers as the student transformer supplies. Different teacher transformers have different load behaviors. Thus, it is necessary to determine the learning weights corresponding to particular teacher transformers. These weights are determined by evaluating customer-level load similarity between the teacher and student transformers using low-resolution load data.

Specifically, for the i 'th customer served by a student transformer, we can obtain a typical daily load pattern, \mathbf{P}_i , which reflects customer behavior and the total capacity of appliances [16]. Then, for a student transformer serving N_c customers, we can obtain N_c daily load patterns, $\{\mathbf{P}_1, \dots, \mathbf{P}_{N_c}\}$. Similarly, for a teacher transformer supplying N_c^k customers, we can obtain N_c^k daily load patterns. Since we have multiple teacher transformers, we can obtain a set of load pattern collections. The load pattern collection for the k 'th teacher transformer is denoted by $\{\mathbf{P}_1^k, \dots, \mathbf{P}_{N_c^k}^k\}$, $k = 1, \dots, N_t$, where, N_t is the total number of teacher transformers. Then, load similarity between a student transformer and the k 'th teacher transformer is evaluated as:

$$W'_k = \frac{1}{N_c N_c^k} \sum_{i=1}^{N_c} \sum_{j=1}^{N_c^k} \|\mathbf{P}_i - \mathbf{P}_j^k\|, \quad k = 1, \dots, N_t, \quad (10)$$

where, N_c^k denotes the number of customers served by the k 'th teacher transformer. Thus, the teacher and student transformers do not necessarily serve the same number of customers. The W'_k 's in (10) are then normalized for a more convenient mathematical representation:

$$W_k = \frac{W'_k}{\sum_{k=1}^{N_t} W'_k}. \quad (11)$$

In summary, the normalized similarity weights reflect the confidence of a student transformer to learn from multiple teacher transformers for load data enrichment.

B. Enriching Load Data

Using the normalized teacher weights, along with the load boundary and variability inference models derived in Section II, we can conduct poor load data enrichment for service transformers that only have SMs.

1) *Inferring Load Boundaries*: In Section II-A, for each teacher transformer with *high-resolution* load data, we have obtained two GPR models for inferring the maximum and minimum loads given the corresponding average load over each low-resolution sampling interval. These two models are non-parametric and expressed in (4). Specifically, the trained maximum load inference model for the k 'th teacher transformer is expressed as:

$$\begin{bmatrix} \bar{P}_k(1) \\ \vdots \\ \bar{P}_k(N) \end{bmatrix} = \begin{bmatrix} f_k(P_{a,k}(1)) \\ \vdots \\ f_k(P_{a,k}(N)) \end{bmatrix} \sim \mathcal{N}(\boldsymbol{\mu}_k, \boldsymbol{\Sigma}_k). \quad (12)$$

To conduct load data enrichment, first, customer-level SM data are aggregated to obtain the load supplied by the student transformer, namely, $\{P_{a,*}(1), \dots, P_{a,*}(N)\}$. Note that

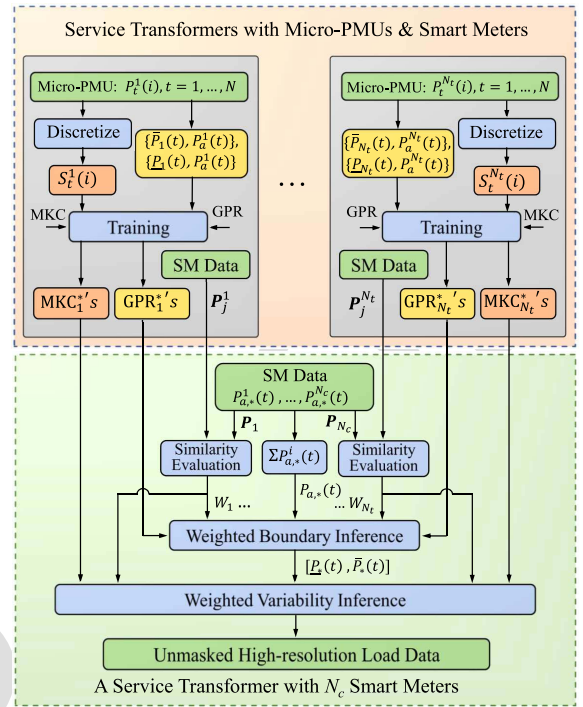


Fig. 7. Detailed steps of enriching load data.

the transformer loss is approximated and added to the aggregate load. Specifically, the total loss of a student transformer supplying an aggregate load, $P_{a,*}(t)$, is estimated as follows:

$$P_{l,*}(t) = P_{nll,*} + \frac{P_{a,*}^2(t)}{P_{rate,*}^2} P_{fl,*}, \quad t = 1, \dots, N, \quad (13)$$

where, $P_{nll,*}$ and $P_{fl,*}$ denote the no-load loss and full-load loss, respectively. $P_{rate,*}$ denotes the kVA rating of the student transformer. $P_{nll,*}$, $P_{fl,*}$, and $P_{rate,*}$ are typically provided by transformer manufacturers. Note that the effect of reactive power is ignored when estimating the loss because the reactive power is typically small [7]. For conciseness, we assume that $P_{a,*}(t)$ in the following sections has already included the aggregate load and the corresponding total loss of the student transformer.

Then, we assume the unknown upper bound of instantaneous load in terms of a function variable, $\bar{P}_{k,*}(t) = f_k(P_{a,*}(t))$, $t = 1, \dots, N$, follows a Gaussian distribution. By appending $\bar{P}_{k,*}(t)$ at the end of (12), an $(N + 1)$ -dimensional Gaussian distribution can be formed as:

$$\begin{bmatrix} \bar{P}_k(1) \\ \vdots \\ \bar{P}_k(N) \\ \bar{P}_{k,*}(t) \end{bmatrix} = \begin{bmatrix} f_k(P_{a,k}(1)) \\ \vdots \\ f_k(P_{a,k}(N)) \\ f_k(P_{a,*}(t)) \end{bmatrix} \sim \mathcal{N}\left(\begin{bmatrix} \boldsymbol{\mu}_k \\ \boldsymbol{\mu}_* \end{bmatrix}, \begin{bmatrix} \boldsymbol{\Sigma}_k & \boldsymbol{\Sigma}_{k*} \\ \boldsymbol{\Sigma}_{k*}^T & \boldsymbol{\Sigma}_{**} \end{bmatrix}\right), \quad (14)$$

where, $\boldsymbol{\Sigma}_{k*}$ represents the training-test set covariances and $\boldsymbol{\Sigma}_{**}$ is the test set covariance. In (14), observations for $\{\bar{P}_k(1), \dots, \bar{P}_k(N)\}$ are known and denoted by $\bar{\mathbf{p}}_k =$

398 $\{\bar{p}_k(1), \dots, \bar{p}_k(N)\}$. Thus, using the Bayes rule, the distri-
399 bution of $\bar{P}_{k,*}(t)$ conditioned on \bar{p}_k is obtained as:

$$400 \quad \bar{P}_{k,*}(t) | \bar{p}_k \sim \mathcal{N}(\mu_*(t), \Sigma_*(t)), \quad (15)$$

401 where, $\mu_*(t) = \Sigma_{k*}^T \Sigma_k^{-1} \bar{p}_k$ and $\Sigma_*(t) = \Sigma_{**} - \Sigma_{k*}^T \Sigma_k^{-1} \Sigma_{k*}$.
402 Note that $\mu_*(t)$ denotes the most probable value of the esti-
403 mated upper bound of instantaneous load given the average
404 load during each low-resolution sampling interval.

405 Since we have N_t teacher transformers, we can obtain
406 a total of N_t estimated maximum load candidates, namely,
407 $\{\mu_*^1(t), \dots, \mu_*^{N_t}(t)\}$. Also, considering load similarity between
408 the student transformer and teacher transformers, a weighted-
409 averaging operation is performed on all the inferred maximum
410 loads to calculate a final estimated upper bound of instanta-
411 neous load:

$$412 \quad \bar{P}_*(t) = \sum_{k=1}^{N_t} W_k \mu_*^k(t), \quad t = 1, \dots, N. \quad (16)$$

413 The same procedure introduced above is also applied to
414 infer the unknown minimum load, $\underline{P}_*(t)$, using the known aver-
415 age load over each low-resolution sampling interval. Once we
416 have obtained the estimated load boundaries, then the trained
417 probability matrices can be leveraged to infer load variability
418 within each boundary.

419 2) *Inferring Load Variability*: As introduced in
420 Section II-B, each teacher transformer has N_d extracted
421 transition matrices corresponding to different load levels.
422 Therefore, the first step in inferring the unknown high-
423 resolution load variability is to determine which transition
424 matrix to use. In other words, we need to find the variability
425 inference matrix corresponding to the load level that the
426 low-resolution load measurement belongs to. This is achieved
427 by splitting the known low-resolution load observations of
428 student transformer into N_d subsets:

$$429 \quad \mathbf{P}_*^j = \{P_{a,*}(t)\}, \quad t \in \{1, \dots, N\}, j = 1, \dots, N_d,$$

$$430 \quad \text{if } F\left(\frac{(j-1) \times 100}{N_d}\right) \leq P_{a,*}(t) < F\left(\frac{j \times 100}{N_d}\right).$$

$$431 \quad (17)$$

432 Then, the j 'th stochastic transition matrix of each teacher
433 transformer is selected for enriching the low-resolution load
434 measurements in the j 'th subset of the student transformer,
435 \mathbf{P}_*^j . Moreover, considering that there is more than one teacher
436 transformer, i.e., for each subset \mathbf{P}_*^j , we have N_t transition
437 matrices to use. Thus, before proceeding to instantaneous
438 load variability inference, a weighted averaging process sim-
439 ilar to the load boundary estimation is conducted to obtain a
440 comprehensive transition modal:

$$441 \quad \mathbf{P}_{r*}^j = \sum_{k=1}^{N_t} W_k \mathbf{P}_r^{j,k}, \quad j = 1, \dots, N_d, \quad (18)$$

442 where, $\mathbf{P}_r^{j,k}$ stands for the transition matrix for the k 'th teacher
443 transformer based on the j 'th subset of observation states,
444 \mathbf{D}_j^k . Then, for each low-resolution load measurement to be
445 enriched, $\mathbf{P}_{a,*}^j(t)$, the final targeted transition matrix, \mathbf{P}_{r*}^j , and
446 the inferred load boundary, $\{\bar{P}_*^j(t), \underline{P}_*^j(t)\}$, are leveraged to

generate the targeted high-resolution load data. Specifically, 447
assume the previous state is $S_{t,*}^j(i-1)$, and the current state 448
is $S_{t,*}^j(i)$, our goal is to determine the next state, $S_{t,*}^j(i+1)$, 449
where, $i = 1, \dots, N'$, stands for the sequence number of states 450
within the t 'th low-resolution sampling interval. To do this, 451
first, a random value at i , $U_*(i)$, is generated from the uni- 452
form distribution within the interval $(0, 1)$. Then, the state at 453
 $(i+1)$ is determined by: 454

$$455 \quad S_{t,*}^j(i+1) = z_*, \quad i = 2, \dots, N' - 1,$$

$$456 \quad \text{if } \sum_{z=1}^{z_*-1} \mathbf{P}_{r*}^j(S_{t,*}^j(i-1), S_{t,*}^j(i), z) \leq U_*(i)$$

$$457 \quad < \sum_{z=1}^{z_*} \mathbf{P}_{r*}^j(S_{t,*}^j(i-1), S_{t,*}^j(i), z). \quad (19)$$

Note that the generated $S_{t,*}^j(i)$'s are discrete state samples, 458
therefore, they need to be transformed to specific load samples: 459

$$460 \quad P_{t,*}^j(i) = \underline{P}_*(t) + \frac{S_{t,*}^j(i)(\bar{P}_*(t) - \underline{P}_*(t))}{N_s},$$

$$461 \quad i = 1, \dots, N'. \quad (20)$$

462 Since there is more than one low-resolution time interval,
463 the above procedure is conducted for *each* low-resolution
464 load observation. Also, since the low-resolution load observa-
465 tions are grouped into multiple subsets, the entire procedure
466 introduced above is conducted through *all subsets* of low-
467 resolution load measurements. The detailed steps for load data
468 enrichment for a student service transformer is illustrated in
469 Fig. 7.

470 IV. CASE STUDY

471 In this section, we have validated the proposed load data
472 enrichment approach using real high- and low-resolution load
473 data [17].

474 A. Dataset Description

475 The dataset includes real 1-second load data for eight
476 service transformers and hourly SM energy data for 185
477 customers. Among these customers, 36 are supplied by the
478 8 transformers with high-resolution load data (with micro-
479 PMUs), and the remaining 149 customers are fed by the other
480 34 service transformers with low-resolution load data (with
481 only SMs). To verify the performance of load data enrich-
482 ment, the utility has also installed extra measuring devices to
483 record 1-second load data for the service transformers with
484 only SMs [17]. The time range of the dataset is two months.
485 In practice, micro-PMUs might have higher sampling rates
486 than one sample per second, however, there is no fundamental
487 difference in verifying the performance of our approach.

488 B. Enriching Low-Resolution Load Measurements

489 Fig. 8 shows one-day actual and enriched 1-second load
490 data for a service transformer. As can be seen, the enriched
491 curve can accurately follow the actual basic load pattern. Note
492 that our goal is not to force the enriched 1-second data to

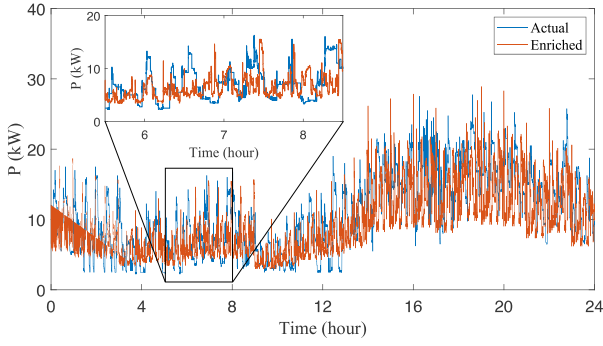


Fig. 8. One-day actual and enriched 1-second load curves.

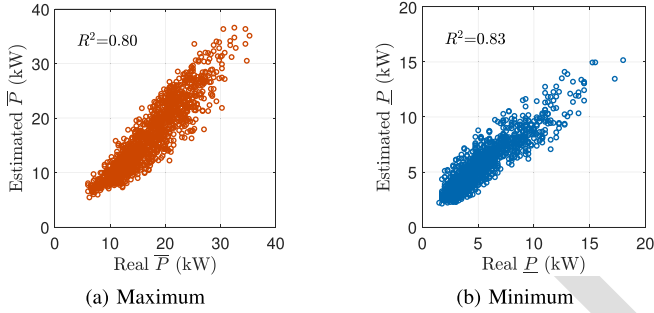


Fig. 9. The estimated maximum and minimum loads against the corresponding actual values.

 TABLE I
 COMPUTED ERROR METRICS OF INFERRING LOAD BOUNDARY

	Maximum AE	Minimum AE	Median AE	RMSE
\bar{P}	3.8	0.01	1.1	1.9
\underline{P}	2.7	0.06	1.1	1.4

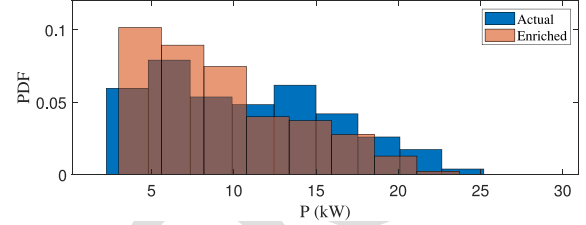


Fig. 10. Distributions of the actual and enriched 1-second load in Fig. 8.

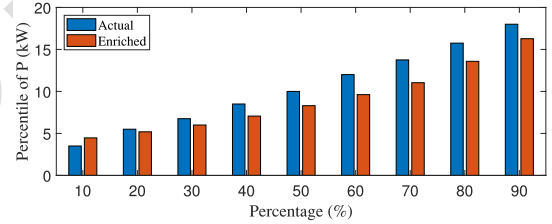


Fig. 11. Percentiles of the actual and enriched 1-second loads in Fig. 8.

493 exactly track the actual load. Instead, our method is designed
 494 to restore the *statistical* properties of instantaneous load given
 495 known low-resolution load observations obtained from hourly
 496 SM data.

497 One critical step of our proposed approach is to determine
 498 the masked maximum and minimum loads given a known
 499 average load observation on an hourly basis. Thus, it is of
 500 significance to examine the performance of the load boundary
 501 inference process. To do this, we have employed the coef-
 502 ficient of determination, R^2 , for fitness evaluation, which is
 503 defined as:

$$R^2 = 1 - \frac{\sum_{i=1}^N (y_i - \hat{y}_i)^2}{\sum_{i=1}^N (y_i - \bar{y})^2}, \quad (21)$$

505 where, y_i denotes the real maximum/minimum instanta-
 506 neous load, \hat{y}_i denotes the corresponding inferred maxi-
 507 mum/minimum instantaneous load, and $\bar{y} = \frac{1}{N} \sum_{i=1}^N y_i$. Fig. 9
 508 illustrates the effectiveness of load boundary estimation, and
 509 it can be seen that the estimated bound shows a linear rela-
 510 tionship with the actual bound. The R^2 values for the upper
 511 and lower bounds are 0.80 and 0.83, respectively. This can
 512 also corroborate the accuracy of our proposed method. To
 513 fully evaluate the performance of our approach on load bound-
 514 ary inference, we have also computed relevant error metrics
 515 based on the high-resolution load in Fig. 8. The error metrics
 516 include the absolute error (AE) and the root mean square error
 517 (RMSE), and the results are summarized in Table I. The error
 518 metrics demonstrate that our method can accurately recover
 519 the unknown upper and lower bounds of the instantaneous
 520 load.

Note that our final goal is to recover the statistical prop-
 erties of the high-resolution load within each low-resolution
 sampling interval. Therefore, the performance of our proposed
 approach needs to be evaluated from the perspective of statist-
 ics. Fig. 10 illustrates the distributions of the actual and
 enriched load samples on the load curves shown in Fig. 8.
 It demonstrates that the enriched load distribution closely
 matches the actual load distribution. In comparison, the non-
 enriched load curve, which only includes 24 load observations,
 cannot sufficiently form a satisfactory distribution. In addition,
 to quantitatively assess load enrichment performance, we
 have examined the differences between the actual and enriched
 load values corresponding to different percentiles, as shown
 in Fig. 11. We have also evaluated the difference between
 the percentiles of the enriched load and the actual load. The
 computed maximum, minimum, median absolute errors of the
 percentiles are 2.7, 0.31, and 1.5, respectively. The RMSE is
 1.6. Therefore, the differences are small, which also proves
 the effectiveness of our proposed approach from a statistical
 perspective.

It is also of interest to examine the results obtained using
 our proposed load data enrichment framework with a *first-*
 order Markov chain model. Fig. 12 presents the actual high-
 resolution load curve and the enriched load curve based on
 a first-order Markov model. To assess the different effects
 of the first- and second-order Markov models on load vari-
 ation inference, we have constructed the distributions of load
 state duration, as shown in Fig. 13, where, D denotes the
 load state duration. By comparing Figs. 13(b) and 13(c) with

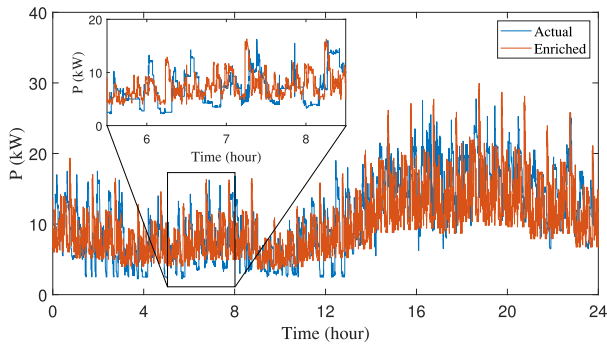


Fig. 12. One-day actual and enriched 1-second load curves (1st-order Markov model).

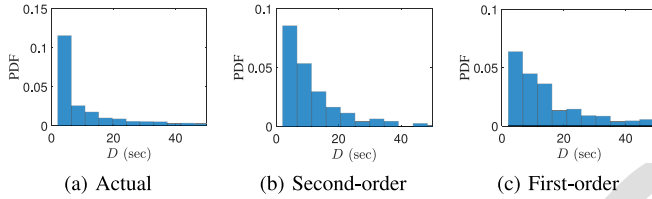


Fig. 13. Distributions of load state duration corresponding to the actual load and the enriched loads.

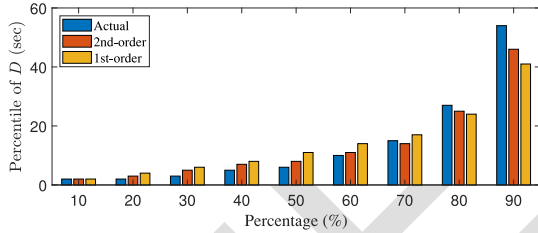


Fig. 14. Percentiles of load state duration corresponding to the actual load and the enriched loads.

550 Fig. 13(a), respectively, we can see that Fig. 13(b) is more sim-
 551 ilar to Fig. 13(a) than Fig. 13(c). This means that our proposed
 552 method can recover the load variation with relatively higher
 553 fidelity compared with the method with a first-order Markov
 554 model. This can also be corroborated by Fig. 14, where,
 555 the percentiles of load state duration corresponding to our
 556 proposed method are closer to the percentiles corresponding
 557 to the actual load.

558 C. Robustness to PV Integration

559 In modern distribution systems, PV integration is common
 560 for utilities. Therefore, it is necessary to test the performance
 561 of our load data enrichment approach under the condition
 562 of PV integration. Specifically, three scenarios are considered
 563 where in all scenarios, both the teacher transformer and the
 564 student transformer supply six customers. In the first scenario,
 565 three of the six customers supplied by the teacher transformer
 566 have installed PVs, and the ratio of the peak PV generation
 567 to the peak load of the teacher transformer is 44%. In the
 568 second scenario, only the student transformer supplies three
 569 PV-installed customers, and the ratio of the peak PV genera-
 570 tion to the peak load of the student transformer is 32%. In the
 571 third scenario, the teacher and student transformers both have

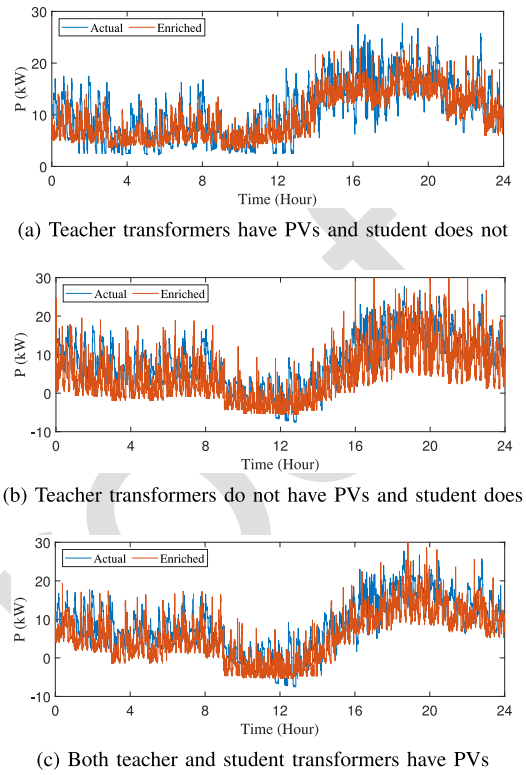


Fig. 15. Robustness of our proposed approach to small-scale PVs.

three PV-installed customers, and the ratios of the peak PV 572
 generation to the peak loads of the teacher and student trans- 573
 formers are 40% and 34%, respectively. The enrichment results 574
 corresponding to the three foregoing scenarios are shown in 575
 Fig. 15. It is demonstrated that the proposed approach can still 576
 achieve accurate high-resolution load data enrichment when 577
 the teacher and/or student transformers serve PV-installed 578
 customers. Quantitatively, for the first scenario, the maximum, 579
 minimum, and median absolute errors between the percentiles 580
 of the enriched load and the actual load are 1.91, 0.23, and 581
 0.96, respectively. For the second scenario, the three computed 582
 error metrics are 3.24, 1.85, and 2.40, respectively. For the 583
 third scenario, the three computed error metrics are 3.24, 1.85, 584
 and 2.40, respectively. In summary, the error metrics demon- 585
 strate that our proposed load data enrichment framework can 586
 adapt to PV integration. 587

588 D. Performing Time-Series Power Flow Studies

589 To thoroughly examine the performance of our proposed 589
 approach, we have conducted time-series power flow studies 590
 by separately feeding the actual and enriched loads into a real 591
 distribution system [18]. The one-line topology of the real 592
 distribution system is shown in Fig. 16. Bus voltages obtained 593
 from power flow analysis, which are critical to distribution 594
 system operators, are used to evaluate our proposed approach. 595
 Specifically, we compare the distributions of bus voltages and 596
 voltage ramps obtained from power flow studies based on the 597
 actual and enriched high-resolution load data, respectively. The 598
 reason for assessing voltage ramp is that voltage ramp is sig- 599
 nificant for renewable energy integration [8]. The voltage ramp 600

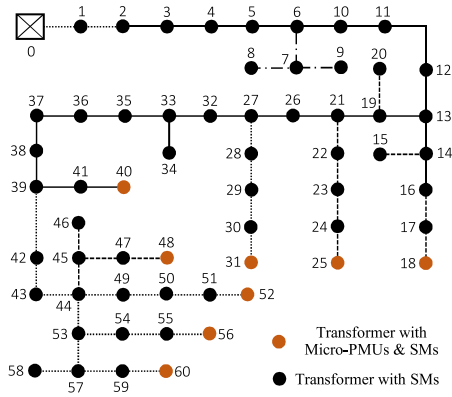


Fig. 16. One-line diagram of a real distribution system.

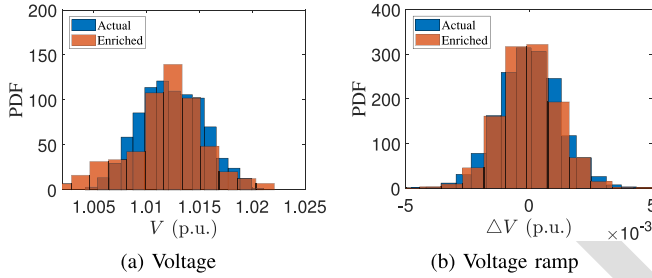


Fig. 17. Distributions of voltage and voltage ramp during a certain hour interval for Bus 57.

ΔV is defined as the difference between the current voltage value and the last voltage value.

Fig. 17 illustrates the distributions of voltages and voltage ramps during a certain hour interval for Bus 57 in the real distribution system. In Fig. 17(a), it is observed that the empirical probability density function (PDF) of voltage based on the actual high-resolution load data can closely fit that based on the enriched high-resolution load data. For comparison, we have also performed a *snapshot* flow study using the average load over the same hour interval. The per-unit voltage for Bus 57 is 1.0124, which is a single value without statistical properties. Therefore, the voltage distribution in Fig. 17(a) fully proves the capability of our proposed approach for recovering statistical characteristics masked by the low-resolution average load measurements. This capability can further enhance distribution system observability and situational awareness. A similar conclusion can be drawn for the voltage ramp, whose distribution is shown in Fig. 17(b). As can be seen, the two voltage ramp distributions corresponding to the real rich load data and the enriched load data closely match each other. In comparison, the single bus voltage value based on the hourly average load cannot demonstrate probabilistic properties. It is important to point out that voltage distribution also depends on the specific structure of distribution systems in addition to specific load observations. For example, if a distribution system has very short line segments and a strong connection with a transmission system, then the bus voltage deviation might not be significant. In contrast, for a weak grid-connected distribution system with long line segments, the loads can have a strong impact on bus voltages.

E. Performance Comparison

It is of significance to compare our approach with other methods presented in previous works. We primarily focus on comparing our approach with an allocation-based methodology introduced in [8] and a noise-based technique presented in [12], which are two primary load data enrichment approaches in previous works.

1) *Comparison With the Allocation-Based Method:* The allocation-based method involves two steps. First, a low-resolution substation- or feeder-level load profile is scaled to obtain service transformer-level load profiles, according to transformer capacity or peak load. Then, the scaled low-resolution load profile is enriched using a variability library, which is constructed by applying the discrete wavelet transform algorithm to known high-resolution transformer-level load measurements. An alternative to scaling low-resolution load profile is to obtain a load pattern obtained by scaling known typical load profiles of other transformers, as presented in [8]. For conciseness, we refer to the techniques presented in [8] as the allocation-based method. The performances of our approach and the allocation-based approach are shown in Figs. 18(a) and 18(b), respectively, where the actual and enriched load curves on a certain day are presented. In Fig. 18(a), we can observe that the basic pattern of the enriched 1-second load can flexibly follow the actual load variation, despite load uncertainty. The superior performance of our approach results from two aspects, the fine spatial granularity of SM data and the design of load boundary inference process. In comparison, the allocation-based load enrichment approach fails to accurately track the basic load pattern, as demonstrated in Fig. 18(b).

The performance of the allocation-based method can also be evaluated by examining the R^2 values computed for the load bounds, as shown in Fig. 19. We can observe that the R^2 values are negative, which means that the estimated maximum/minimum bound offers a poor estimation of the variation of the actual maximum/minimum bound. The unsatisfying performance of the allocation-based approach can also be viewed by observing the two scatter plots in Fig. 19, where, most scatters are located above the upper-right diagonal line, indicating an overestimation of the actual load bounds.

To further evaluate the performance of our approach and the benchmark methods, we have also computed the cumulative probability of the actual and enriched load presented in Fig. 18. The empirical cumulative distribution functions (ECDFs) are illustrated in Fig. 21, where, we can observe that the ECDF corresponding to our method is much closer to the ECDF of the actual load than the ECDF corresponding to the allocation-based method. To quantitatively assess the similarity between the two ECDFs, we have computed the two-sample Kolmogorov-Smirnov (KS) statistic for each method, using the following equation:

$$D = \sup_P |F_a(P) - F_e(P)|, \quad (22)$$

where, \sup denotes the supremum of the set of distances. $F_a(P)$ denotes the ECDF of the actual high-resolution load, and $F_e(P)$ denotes the ECDF of the enriched load. Intuitively,

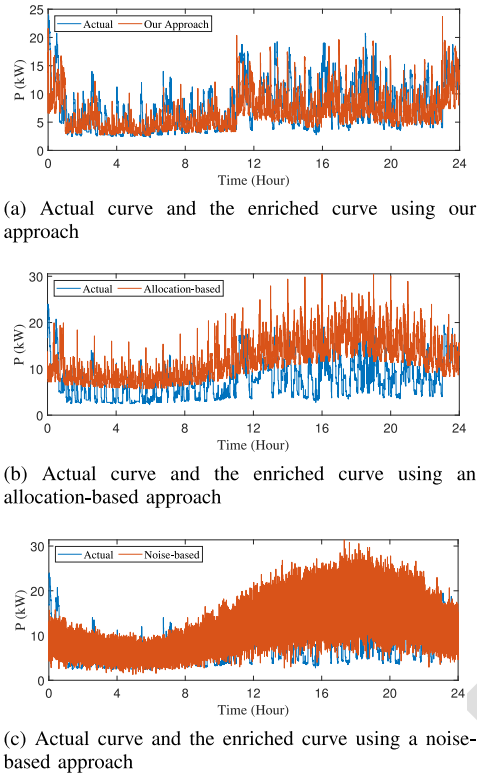


Fig. 18. The actual high-resolution load curve and the enriched load curves.

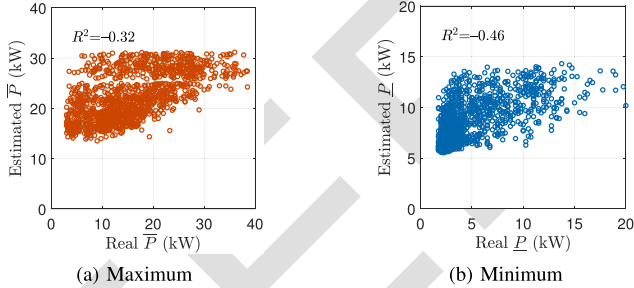


Fig. 19. The estimated maximum and minimum load bounds obtained from the allocation-based method against the corresponding actual values.

D measures the largest pairwise absolute distance between the ECDFs of the actual load and the enriched load. In Fig. 21, we can observe that the two-sample KS statistic for our method is 0.14, which is significantly smaller than the statistic for the allocation-based method, which is 0.40.

2) *Comparison With the Noise-Based Method:* The basic idea of the noise-based approach is to add Gaussian noise to a typical or known low-resolution load profile. Fig. 18(c) shows the actual 1-second load curve and the enriched load curve obtained by the noise-based approach. One primary shortcoming of the noise-based approach is that it can not faithfully capture the cyclicity of the load state. This shortcoming can be observed in Fig. 18(c), where, the enriched load curve clutters the plot and does not present a clear duration of load state. The unsatisfactory performance of the noise-based approach can also be corroborated by Fig. 20, where, the negative R^2 values demonstrate poor explanations of the inferred maximum/minimum load bound on the actual load bound. The

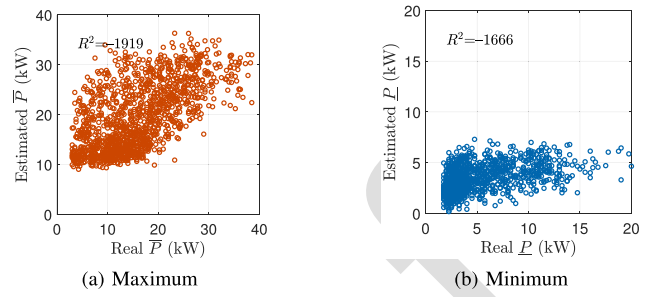


Fig. 20. The estimated maximum and minimum load bounds obtained from the noise-based method against the corresponding actual values.

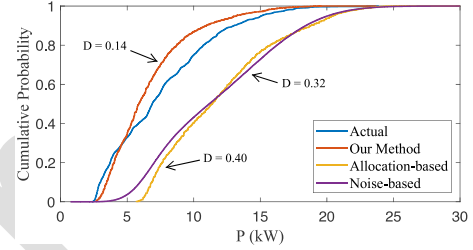


Fig. 21. Cumulative probability distributions of the actual load and the enriched load in Fig. 18.

TABLE II
COMPUTED ERROR METRICS BASED ON LOAD CURVES IN FIG. 18

	Our Approach	Allocation-based	Noise-based
nMAE (%)	12.3	22.8	21.9
nRMSE (%)	16.4	28.1	27.5

computed D value for the noise-based method is 0.32, which is greater than 0.14, as shown in Fig. 21. This demonstrates that our method has a better performance than the noise-based method in terms of the two-sample KS statistic.

To quantitatively compare the aforementioned three approaches, we have also computed the normalized mean absolute error (nMAE) and the normalized root mean square error (nRMSE) based on the load curves in Fig. 18. Specifically, nMAE and nRMSE are computed as follows:

$$nMAE = \frac{\sum_{t=1}^{n_t} |P(t) - \hat{P}(t)|}{P_{max}} \times 100\%, \quad (23)$$

$$nRMSE = \frac{\sqrt{\sum_{t=1}^{n_t} (P(t) - \hat{P}(t))^2}}{P_{max}} \times 100\%, \quad (24)$$

where, n_t is the total number of samples in a day with a resolution of 1 second, i.e., 86400. $P(t)$ and $\hat{P}(t)$ denote the actual and estimated loads at time t , respectively. P_{max} denotes the peak of the actual load. The computed error metrics are summarized into Table II. We can see that compared to the allocation- and noised-based methods, our approach has smaller errors.

V. CONCLUSION

This paper is devoted to temporally enriching low-resolution load data for service transformers that only have SMs, using

high-resolution load data from service transformers with micro-PMUs and SMs. The entire process includes two stages, determining the maximum and minimum load bounds using known low-resolution load measurements and trained regression models, and inferring load variability within load boundaries using trained probabilistic transition models. The regression and transition models are trained using high-resolution load data from service transformers with micro-PMUs. We have used real high-resolution load data to prove that our approach is able to accurately recover high-resolution load data masked by the average load measurements over low-resolution sampling intervals. The enriched high-resolution load data can significantly enhance utilities' grid-edge observability and situational awareness of distribution systems. Our paper's key findings are summarized as follows.

- The 1-second load within an hourly interval can be 40% times larger or smaller than the corresponding average load during the same hour interval. By performing power flow studies, we have found that using the hourly average load for conducting power flow analysis cannot accurately capture the actual condition of distribution systems. Therefore, performing low-resolution power flow studies might cause significant errors, especially for those distribution networks that have a weak grid connection and long line segments.
- The numerical experiments have verified that our proposed approach shows strong robustness and adaptability to PVs.
- The numerical experiments have also demonstrated that our approach can accurately recover statistical properties of the instantaneous load within each low-resolution sampling interval of SM. The power flow studies show that our approach can faithfully reflect distribution system's actual voltage conditions from a statistical perspective.

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